# Precipitation and magnetic models coupling for magnetic aging prediction

Fabien Dancoisne<sup>a, b</sup>, Myriam Dumont<sup>a</sup>, Stéphane Clénet<sup>b</sup>, Abdelkader Benabou<sup>b</sup>

<sup>a</sup>Arts & Métiers Institute of Technology. (MSMP-EA7350) Mechanics, Surfaces and Materials Processing, 8 bd Louis XIV, Lille Cedex, 59046, France <sup>b</sup>Univ. Lille, Arts & Métiers Institute of Technology, Centrale Lille, HEI. (L2EP-EA2697) Laboratoire d'Électrotechnique et d'Électronique de Puissance, Bâtiment ESPRIT, Avenue Henri Poincaré, Villeneuve d'Ascq, 59655, France

While in operation, widely-used electrical machines are not yet capable of converting all the input energy, thus resulting in a waste of energy. Within magnetic cores, the heat-dissipated iron losses pose a serious threat to energy efficiency. With Non-Oriented Electrical Steels (NOES) as the main material they are conceived with, it is of prime interest to understand and harness the irreversible consequences the operating temperature (between  $160^{\circ}C \& 200^{\circ}C$ ) may have on magnetic performances. In fact, the losses increase over time is due to a precipitation mechanism at the microscopic scale: the magnetic aging. This paper proposes a multi-scale and multi-physics model that accounts for the effects of precipitation on iron losses and that is based on a combination of the JMAK and Jiles-Atherton's models.

Keywords: NOES; Magnetic Aging; Hysteresis; Precipitation

## 1. Introduction

Magnetic aging refers to an irreversible degradation of magnetic performances that appears when electrical steels are subjected to moderate temperatures during machine operation, usually between 160°C and 200°C. When specific material composition and microstructural conditions are met [1-2], this heat-dissipation phenomenon, in turn, causes carbon atoms present in the alloy lattice to precipitate, forming large particles hindering magnetization. In the literature, the effects of aging are well characterized [1], as well as their impacts on magnetic properties, such as coercive field [2] and iron losses [3]. In general, the more carbon there is, the higher the precipitate's volume fraction [4], the higher the drawbacks on performances. In this communication, a mutli-physics model accounting for precipitation in electrical steels is proposed. A first section will deal with the characterization method used on lab-cast samples, whose results will be explored in the next part so to build a multi-scale model coupling precipitation kinetics (JMAK model [3]) and static magnetic hysteresis (Jiles-Atherton's model [5]). For this study, several materials of known chemical composition will be considered. Lastly, the modeling suitability will be discussed and further developments mentioned.

## 2. Experimental methodology

Magnetic aging of Fe-Si alloy samples is characterized as follows: first,  $200 \times 30 \times 0.25$  mm samples are placed in an oven for a set amount of time (several hours) and undergo an isothermal heating at 160, 180 or  $200^{\circ}$ C. They are then taken out and their magnetic properties are measured at room temperature, at 5 and 50 Hz by means of a Single Strip Tester (SST) device. The chemical compositions of the studied samples feature different amounts of silicon and carbon.

## 3. Multi-scale model

The multi-scale model consists in applying the JMAK model to the evolution over time of the transformation rate Y(t) linked to precipitation mechanisms. Since precipitates act as pinning sites for domain walls movements during magnetization, it can be represented by the pinning factor parameter k (1) of the Jiles-Atherton (J-A) model of magnetic hysteresis.

$$\frac{dM_{\rm irr}}{dH_e} = \frac{M_{\rm an} - M_{\rm irr}}{\pm k} \tag{1}$$

Where  $M_{irr}$  is the irreversible part of magnetization,  $H_e$  the effective field and  $M_{an}$  the anhysteretic magnetization. The analysis of experimental data shows that the pinning factor evolution resembles that of the transformation rate, leading to its approximation of eq. (2).

$$k(t) = Y_k(t) \times \Delta k + k_{\min}, \qquad (2)$$

An application of the coupled approach is shown on fig. 1 and displays a satisfactory result between experimental and simulated B(H) loops after a 96-hour aging at 200°C.



Figure 1: Hysteresis loop of a Fe-Si sample aged at 200°C for 96 hours.  $B_{max}=$  1.5 T,  $f=5\ Hz$ 

### References

[1] S. Ray, "Magnetic ageing characteristics of low silicon electrical steels", Journal of Magnetism and Magnetic Materials, 28, 1982.

[2] L.J. Dijkstra, C. Wert, "Effect of inclusions on coercive force of iron", Phys. Rev. 79 (6), 1950.

[3] M. Jamil and al., "Application of the JMAK precipitation law in iron loss modelling to account for magnetic ageing effect" J.M.M.M., vol. 547, 2022.

[4] J.R. de Oliveira-Junior and al., "Kinetics of magnetic ageing of 2% Si non-oriented grain electrical steel", Mater. Res., 21 (1), 2018.

[5] D.C. Jiles and D.L. Atherton, "Theory of ferromagnetic hysteresis", J. Appl. Phys., 1984

Acknowledgements: ANR-PRC Mastermind2